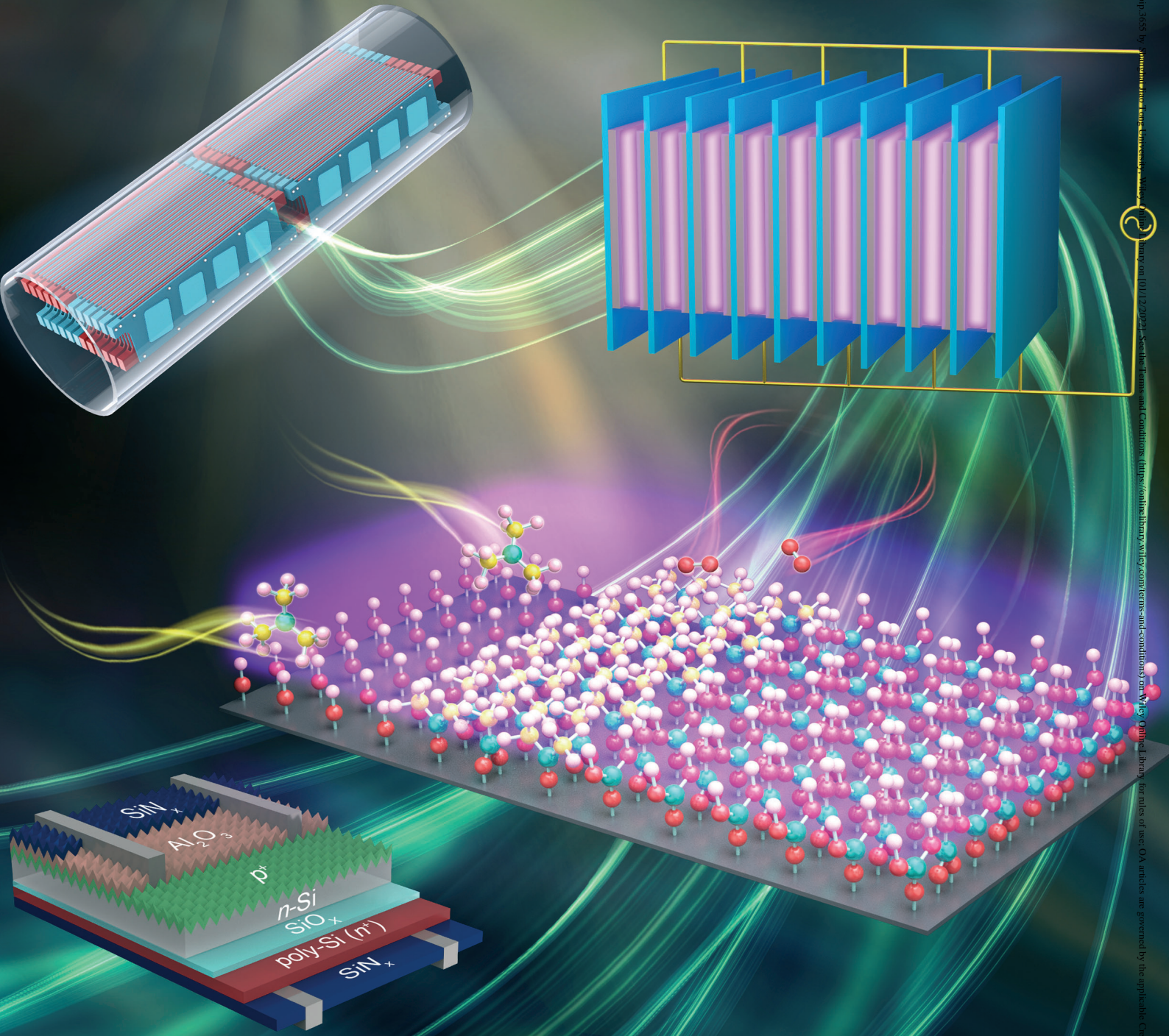


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# Tube-type plasma-enhanced atomic layer deposition of aluminum oxide: Enabling record lab performance for the industry with demonstrated cell efficiencies >24%

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## Abstract

In this work, single-side aluminum oxide (Al<sub>2</sub>O<sub>3</sub>) deposition enabled by a new tube-type industrial plasma-assisted atomic layer deposition (PEALD) technique is presented to meet the increasingly stringent requirements for high-efficiency solar cell mass production. Extremely low emitter saturation current densities,  $J_{0e}$ , down to 15 fA/cm<sup>2</sup> are achieved on an industrial textured boron emitter with a sheet resistance of 104 Ω/sq, passivated by PEALD Al<sub>2</sub>O<sub>3</sub>/PECVD SiN<sub>x</sub> stack after firing. An implied open-circuit voltage of up to 721 mV is obtained on symmetrical lifetime samples. The underlying passivation mechanisms of this new tube-type PEALD Al<sub>2</sub>O<sub>3</sub> are investigated by contactless corona-voltage measurements. The results indicate that the superior passivation is mainly attributed to a low interface defect density down to  $1.1 \times 10^{11} \text{ cm}^{-2} \text{ eV}^{-1}$  and a high negative fixed charge density up to  $4.5 \times 10^{12} \text{ cm}^{-2}$ . Simulations show that the obtained  $J_{0e}$  is close to its intrinsic limit. Lastly, the developed tube-type PEALD Al<sub>2</sub>O<sub>3</sub> is applied to industrial TOPCon solar cells achieving an average cell efficiency above 24% and a maximum  $V_{oc}$  of 707 mV. This work shows that the record level of surface passivation available from lab-scale PEALD reactors is now available in a flexible high-throughput industrial PEALD platform, which opens a new route for mass production of high-efficiency industrial TOPCon solar cells with a lean process at low costs.

## KEYWORDS

aluminum oxide, boron emitter passivation, industrial tube PEALD, interface oxide, TOPCon



## 1 | INTRODUCTION

The current mainstream industrial crystalline silicon (*c*-Si) solar cell is based on the passivated emitter and rear cell (PERC) technology, which was first introduced in the late 1980s with an efficiency of 22.8%<sup>1</sup> and achieved a record efficiency of 25% with the passivated emitter and rear local contact (PERL) structure in the late 1990s.<sup>2</sup> In recent years, the PERC cells have been well developed, with a mass production average cell efficiency of ~23% in 2021 and a champion efficiency of 23.83% for a commercial *p*-type Czochralski (Cz) PERC cell reported by Longi solar in the 2020s.<sup>3</sup> However, this cell performance is approaching its practical limit.<sup>2,4–8</sup> The efficiency of the industrial PERC cell is limited by the recombination losses at the metal contacts and recombination in the *c*-Si bulk.<sup>9</sup> Passivating contacts have been proposed to reduce the losses due to the metal contacts for the next-generation industrial high-efficiency silicon solar cells.<sup>5,10–12</sup> The best-known example of a solar cell with passivating contacts for both electrons and holes is the heterojunction with intrinsic thin layer (HIT) solar cell<sup>13–20</sup> with a record efficiency of 25.54%<sup>21</sup> for a bifacial solar cell and 26.7%<sup>19</sup> in an interdigitated back contact (IBC) design. Another good example is the tunnel oxide passivated contact (TOPCon) solar cell,<sup>10,22–31</sup> which features a passivating electron contact with a record efficiency of 25.8%<sup>25</sup> on *n*-type *c*-Si, 26.0%<sup>32</sup> on *p*-type *c*-Si, and 26.1%<sup>33</sup> for an IBC solar cell. Unlike the HIT solar cell, the TOPCon solar cell fabrication process is compatible with the well-developed PERC solar cell fabrication technology, making it the ideal candidate for upgrading existing PERC lines.

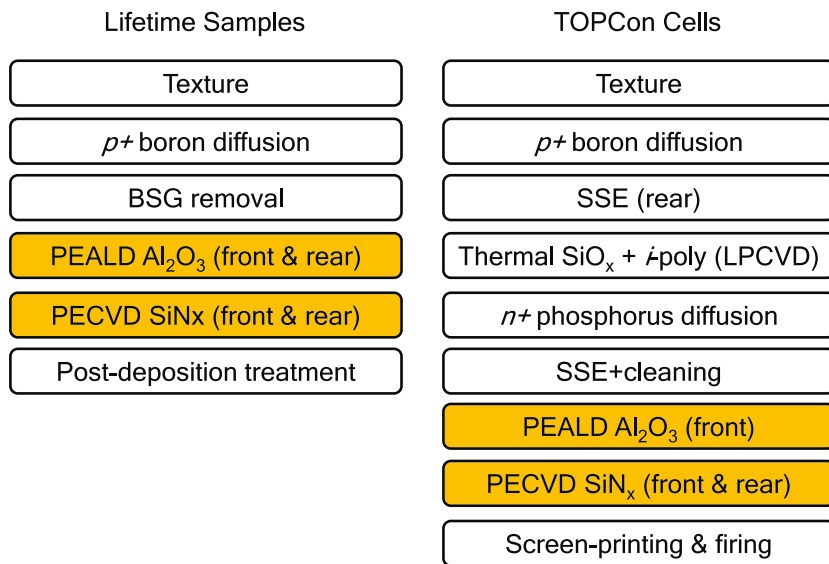
Instead of the *p*-type wafers used for the vast majority of PERC cells, *n*-type *c*-Si wafers are commonly used for industrial TOPCon solar cells. They have a higher bulk lifetime, are less sensitive to most metal impurities, and do not suffer from boron-oxygen related degradation.<sup>34–36</sup> In addition, excellent surface passivation with a surface saturation current density ( $J_0$ ) lower than 5 fA/cm<sup>2</sup><sup>28,37</sup> can be achieved for the passivating electron contact at the rear of a TOPCon solar cell. The TOPCon solar cell efficiency is currently limited by recombination at the front boron-doped surface,<sup>25,32</sup> which also has a larger surface area due to the pyramid textured front of the solar cell. Negatively charged aluminum oxide (Al<sub>2</sub>O<sub>3</sub>) is the ideal candidate to passivate the *p*-type boron emitter surface.<sup>38–42</sup> To date, the photovoltaic industry is predominantly using plasma-enhanced chemical vapor deposition (PECVD) or thermal atomic layer deposition (ALD) for the deposition of the Al<sub>2</sub>O<sub>3</sub> films. Unfortunately, the level of surface passivation on highly doped *p*-type *c*-Si provided by industrial PECVD and thermal ALD Al<sub>2</sub>O<sub>3</sub> is limiting the performance of TOPCon solar cells due to its high sensitivity of recombination at the front surface. The best results in the lab on highly doped *p*-type *c*-Si have been obtained by plasma-enhanced atomic layer deposited (PEALD) Al<sub>2</sub>O<sub>3</sub> due to its relatively high fixed charge density ( $Q_f$ ) compared with Al<sub>2</sub>O<sub>3</sub> films grown by other deposition techniques.<sup>43</sup> PEALD shares all the intrinsic advantages of ALD technology, such as precise thickness control, excellent uniformity, and conformity over large areas, making it an ideal deposition method for any textured surface.<sup>44,45</sup> However, the main drawback of the ALD method for solar

cell manufacturing is the difficulty of avoiding wrap-around deposition, which can result in challenges in the rear metallization and rear optics.

In this work, we will present a novel industrial low-cost high-throughput single-side tube-based PEALD Al<sub>2</sub>O<sub>3</sub> process. This PEALD process can be integrated into tube-PECVD systems commonly used in the manufacturing of PERC cells and are popular for its low cost of ownership (COO) due to lower equipment cost, smaller footprint, higher uptime, and low maintenance cost. These tube-type PEALD/PECVD would feature different tubes for different deposition technology and would significantly simplify the manufacturing complexity and reduce the cost compared with the current standalone thermal ALD Al<sub>2</sub>O<sub>3</sub> system plus the tube-type PECVD SiN<sub>x</sub> system for TOPCon application. Extremely low  $J_{0e}$  values down to 14.6 fA/cm<sup>2</sup> and  $iV_{oc}$  up to 721 mV were achieved on an industrial textured boron emitter with a sheet resistance of 104 Ω/sq. The underlying passivation mechanism of the tube-type PEALD Al<sub>2</sub>O<sub>3</sub> was investigated by contactless corona-voltage measurements. The results indicated that the superior passivation was mainly attributed to a low interface defect density  $D_{it}$  (down to  $1.1 \times 10^{11}$  cm<sup>-2</sup> eV<sup>-1</sup>) and a high fixed charge density  $Q_f$  (up to  $-4.5 \times 10^{12}$  cm<sup>-2</sup>). Simulation shows that the obtained  $J_{0e}$  values were very close to their intrinsic limit value, where  $J_{0e}$  is solely ruled by Auger recombination in the boron emitter. Lastly, the developed tube-type PEALD Al<sub>2</sub>O<sub>3</sub> was applied to industrial TOPCon solar cells, and an average cell efficiency above 24% with a maximum  $V_{oc}$  of 707 mV was obtained. This work shows that record lab-scale performance is now available in a high-throughput industrial tool, making tube-type PEALD Al<sub>2</sub>O<sub>3</sub> a strong candidate for boron emitter passivation for TOPCon solar cells.

## 2 | EXPERIMENTAL DETAILS

To investigate the level of surface passivation, symmetrical lifetime samples were prepared based on the process flow shown in Figure 1. G12-sized (170 μm, 441 cm<sup>2</sup>) Czochralski (Cz) *n*-type silicon wafers with a resistivity of 0.3 to 2.1 Ω·cm were used. The wafers were firstly saw damage etched (SDE) in potassium hydroxide (KOH) followed by an alkaline texturing on both sides of the wafer, resulting in a pyramid size of ~2 μm. After cleaning, boron diffusion was performed in a tube furnace using boron trichloride (BCl<sub>3</sub>) as dopant source, thus resulting in a symmetrical  $p^+np^+$  structure with an emitter sheet resistance of ~104 Ω/sq. Subsequently, the borosilicate glass (BSG) layer was stripped in a diluted (10%) hydrofluoric acid (HF) solution until the surface became hydrophobic. After cleaning, a ~3 nm Al<sub>2</sub>O<sub>3</sub> film was deposited on both sides of the samples using a tube-type PEALD system (ZR5000, LeadMicro, 480 pcs/tube for 210 mm wafers, 6 tubes/system, throughput ~9000 pcs/h). For the PEALD Al<sub>2</sub>O<sub>3</sub> process, trimethylaluminum (TMA) [Al (CH<sub>3</sub>)<sub>3</sub>] (solar grade 5N, Nata Opto-electronic Material) was used as the aluminum precursor, and an O<sub>2</sub> plasma was used as the oxidant, generated by a direct radio frequency (RF) plasma source operating at 40 kHz and a power of 12 kW. The growth-per-cycle (GPC) was ~1.14 Å/cycle, the pulse

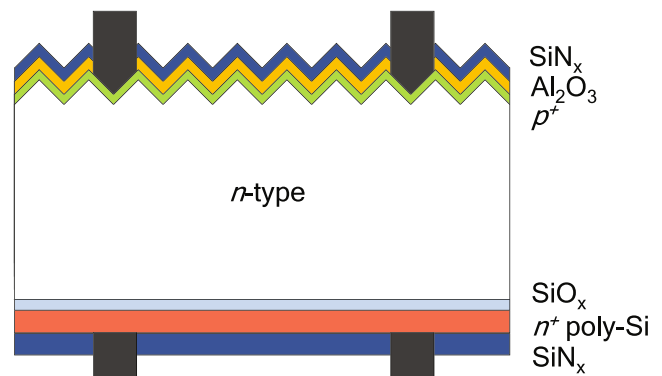


**FIGURE 1** The fabrication process flows for the lifetime samples and the bifacial TOPCon silicon solar cells

time for both TMA and  $\text{O}_2$  plasma was about 4 s, and the cycle time was  $\sim 25$  s; 30 ALD cycles were used to achieve a 3-nm  $\text{Al}_2\text{O}_3$  film. All films were deposited at a substrate temperature of  $200^\circ\text{C}$ . Subsequently, a  $\sim 70$  nm  $\text{SiN}_x$  film was deposited on both sides of the samples in a different tube of the same PECVD reactor. After that, the symmetrical samples underwent a rapid thermal anneal in an industrial fast firing furnace for a few seconds (set peak temperature  $800^\circ\text{C}$ ), followed by an industrial light-induced annealing furnace (light soaking) for a few seconds.

To verify the performance of the developed industrial tube-type PEALD  $\text{Al}_2\text{O}_3$  passivation at the device level, industrial TOPCon cells were fabricated based on the process flow shown in Figure 1, and the resulting cell structure is shown in Figure 2. After SDE and texturing on both sides, boron diffusion was carried out to form a  $p^+$  layer. Subsequently, an inline single-side etch (SSE) was performed to remove the  $p^+$  doping and polish the rear surface. After cleaning, an interfacial thermal oxide and an intrinsic polysilicon ( $i$ -poly) layer were deposited at the rear surface by an industrial low-pressure chemical vapor deposition (LPCVD) tool. Phosphorus diffusion was carried out to dope the  $i$ -poly layer and form the  $n^+$  polysilicon layer. Subsequently, an inline single-side etch (SSE) was performed to remove the wrap-around  $n^+$  layer at the front surface. After cleaning, the front  $p^+$  surface was passivated by a thin film stack consisting of  $\sim 3$ -nm PEALD  $\text{Al}_2\text{O}_3$  film and  $\sim 70$ -nm PECVD  $\text{SiN}_x$  film, while the rear surface was coated with a  $\sim 70$ -nm  $\text{SiN}_x$  film. All thin films were deposited by an industrial tube-type PEALD/PECVD system (ZR5000, LeadMicro). Lastly, the samples were screen-printed on both sides with an Al-Ag alloy paste for the front and Ag paste for the rear (both with 12 busbars). The cells were then fired at a peak temperature of around  $800^\circ\text{C}$  (set temperature was used, unless stated otherwise) using an industrial fast-firing furnace, followed by an illuminated anneal in an industrial furnace for a few seconds.

The passivation quality of the  $\text{Al}_2\text{O}_3$  film was quantified by measuring the effective minority charge carrier lifetime of the symmetrically passivated  $p^+np^+$  structures using a contactless



**FIGURE 2** Schematic of a tube-type PEALD  $\text{Al}_2\text{O}_3$  passivated  $n$ -type bifacial TOPCon silicon solar cell

photoconductance decay (PCD) tester (WCT-120, Sinton Instruments). The implied open-circuit voltage ( $iV_{oc}$ ) of the samples was extracted according to the method published by Sinton and Cuevas.<sup>46</sup> The emitter saturation current density ( $J_{oe}$ ) was determined according to the high-injection method proposed by Kane and Swanson<sup>47</sup>:

$$\frac{1}{\tau_{eff}} = \frac{1}{\tau_{Auger}} = \frac{1}{\tau_{SRH}} + \frac{2J_{oe}(N_d + \Delta n)}{qn_i W} \quad (1)$$

where  $\tau_{eff}$  is the measured effective carrier lifetime of the sample,  $\tau_{Auger}$  the intrinsic Auger lifetime,<sup>48</sup>  $\tau_{SRH}$  the defect-related Shockley-Read-Hall bulk lifetime,  $N_d$  the bulk doping concentration,  $\Delta n$  the excess carrier density,  $q$  the elementary charge,  $n_i$  the intrinsic carrier concentration, and  $W$  the sample thickness. The presented  $J_{oe}$  values were evaluated at  $25^\circ\text{C}$ , with a corresponding  $n_i$  of  $8.6 \times 10^9 \text{ cm}^{-3}$ .<sup>49,50</sup> The measurements of  $J_{oe}$  to be accurate within 3% to 7%.<sup>51</sup> The emitter sheet resistance was determined by a four-point probe measurement. The active dopant depth profile was

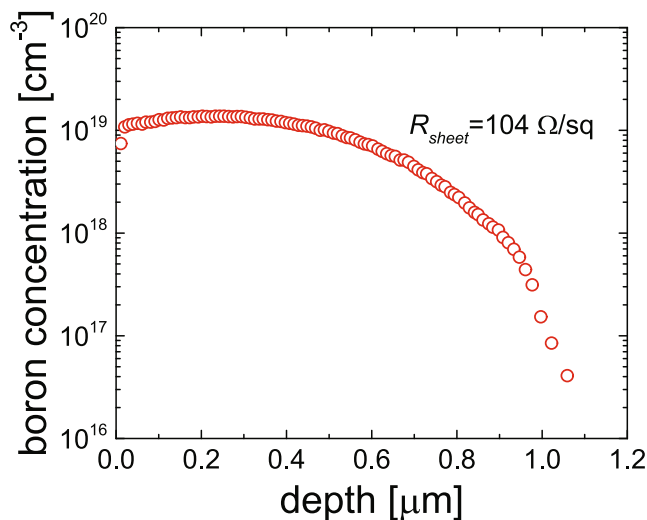
measured by electrochemical capacitance-voltage (ECV) profiling (WEP, CVP21). The surface passivation mechanism and the interface properties were studied by using contactless corona-voltage (C-V) measurements (PV2000, Semilab). Undiffused  $n$ -type planar samples with 10-nm PEALD  $\text{Al}_2\text{O}_3$  films on both sides were used. These measurements are not feasible on highly doped samples as the applied corona charge will be screened by the highly conductive diffused layer so that a transition from accumulation to inversion (which is needed for  $Q_f$  and  $D_{it}$  evaluation) can no longer take place. The procedure of determination of the fixed charge density ( $Q_f$ ) and the energy-level dependent interface defect density  $D_{it}(E)$  from the contactless C-V measurements is discussed in detail elsewhere.<sup>52–54</sup> The ECV and contactless C-V results were used to model the theoretical  $J_{0e}$  using EDNA 2 from PV Lighthouse.<sup>55</sup> The commonly used physical models to describe silicon wafer-based solar cells such as carrier mobility model by Klaassen,<sup>56,57</sup> intrinsic bandgap by Passler,<sup>58</sup> the density of states from Sentaurus, dopant ionization by Altermatt,<sup>59</sup> Fermi-Dirac statistics,<sup>60,61</sup> bandgap narrowing by Schenk,<sup>62</sup> and the effective intrinsic carrier density by Altermatt,<sup>63</sup> were used in the simulations. The radiative recombination was modeled using the model proposed by Trupke et al.<sup>64</sup> As the emitter region was heavily doped, we assumed no Shockley-Read-Hall (SRH) recombination in the emitter, and the calculation of the surface SRH was done according to McIntosh et al.<sup>65</sup> The empirical Auger parameterization model by Richter<sup>66</sup> was used to model Auger recombination in the emitter and bulk. Full-area current-voltage ( $I$ - $V$ ) measurements were conducted using a *Halm* inline measurement system (cetisPV-IUCT-3600-BF) calibrated using a reference cell from Fujian Metrology Institute, National PV Industry Measurement and Testing Center.

### 3 | RESULTS AND DISCUSSION

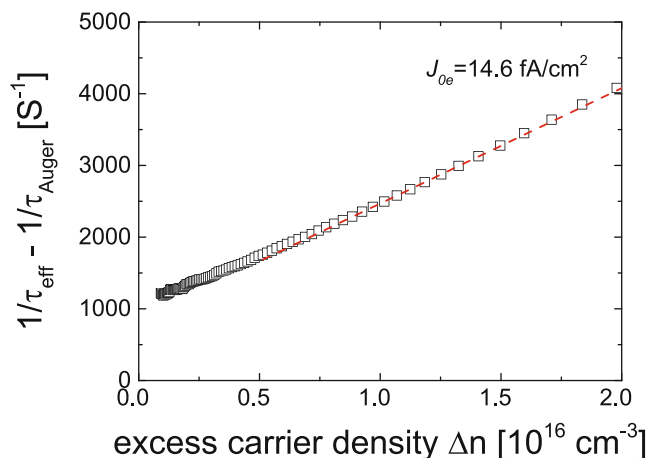
#### 3.1 | Experimental results on symmetrically passivated textured boron emitters

The boron emitter dopant profile was measured by ECV and the result is shown in Figure 3. The emitter had a surface doping concentration of  $\sim 7.4 \times 10^{18} \text{ cm}^{-3}$  and a junction depth of  $\sim 1.1 \mu\text{m}$ . The sheet resistance of the emitter was  $\sim 104 \Omega/\text{sq}$  as determined by a four-point probe measurement. The measured Auger-corrected inverse effective minority carrier lifetime for light-soaked  $p^+/n/p^+$  samples, symmetrically passivated by 3-nm  $\text{Al}_2\text{O}_3$  and 70-nm  $\text{SiN}_x$  stack is shown in Figure 4. A linear relation between the Auger-corrected inversion lifetime and the injection carrier density was obtained from moderate to high injection levels [ $(0.5\text{--}2.0) \times 10^{16} \text{ cm}^{-3}$ ]. Hence,  $J_{0e}$  could be extracted from the slope of the linear function according to Equation (1). In this work,  $J_{0e}$  was extracted at an injection level of  $1 \times 10^{16} \text{ cm}^{-3}$ , and the corresponding  $J_{0e}$  values were in the range of 15 to 19  $\text{fA}/\text{cm}^2$ .

The measured effective lifetime and the corresponding  $iV_{oc}$  for the symmetrically passivated textured  $p^+/n/p^+$  samples after firing and light soaking treatment are shown in Figure 5. An average

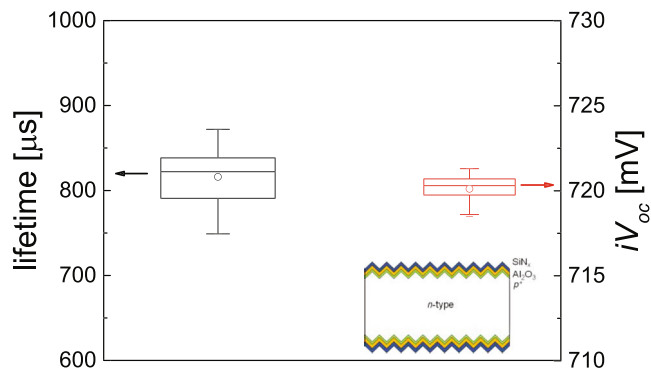


**FIGURE 3** Active boron depth profile of the  $p^+$  emitter as determined by ECV. The sheet resistance determined by four-point probe measurement is also shown

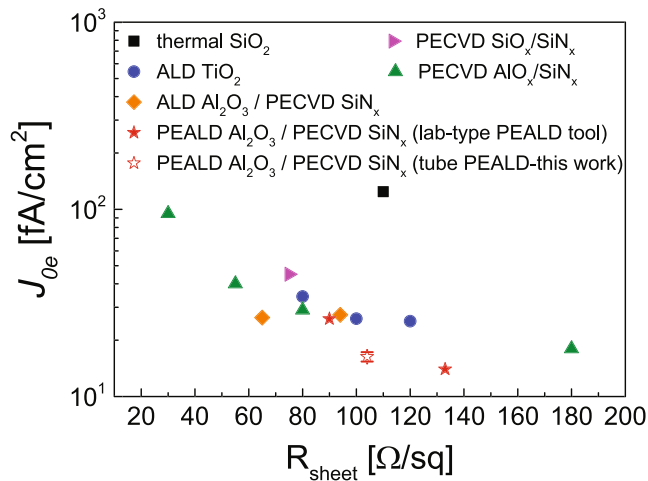


**FIGURE 4** Measured Auger corrected inverse effective minority charge carrier lifetime as a function of the injection level for symmetrical textured  $p^+/n/p^+$  samples symmetrically passivated by 3-nm  $\text{Al}_2\text{O}_3$ /70-nm  $\text{SiN}_x$  stack after firing and light soaking treatment. The solid line is a linear  $J_{0e}$  that fits the measured data

effective lifetime value of 816  $\mu\text{s}$  with corresponding  $iV_{oc}$  up to 721 mV was achieved. The state-of-the-art  $J_{0e}$  values reported for other deposition methods on textured boron emitters are shown in Figure 6 and compared with the results obtained in this work. Only results on textured samples are shown to ensure an apples-to-apples comparison. It should be noted that the Auger- and defect-related recombination in the various boron emitters used in the various studies could be significantly different due to differences in the process conditions used. As can be seen, excellent boron emitter passivation

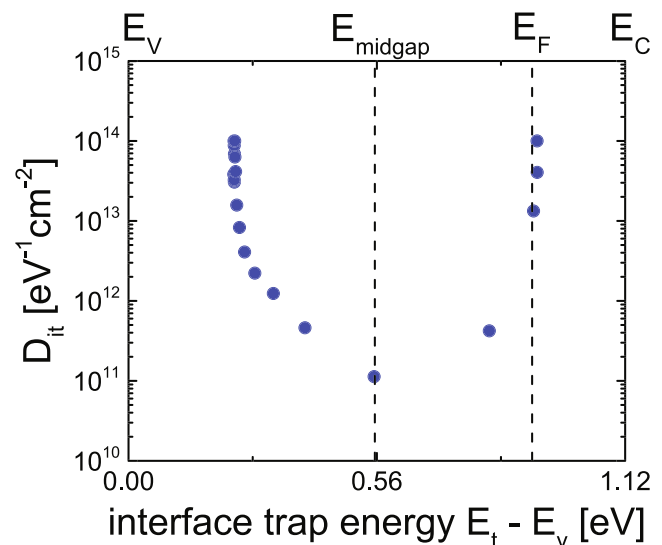


**FIGURE 5** Measured lifetime values (left axis) and corresponding implied  $V_{oc}$  values (right axis) of symmetrical textured boron emitter samples after firing and light soaking treatment. Eight samples were prepared and five points (center and four corners) were measured on each sample. Boxes, 25–75% range; vertical lines, maximum and minimum; horizontal lines within boxes, median; circle shape within boxes, mean



**FIGURE 6** Measured emitter saturation current density  $J_{0e}$  as a function of boron emitter sheet resistance passivated by an industrial tube-type system PEALD  $\text{Al}_2\text{O}_3/\text{PECVD SiN}_x$  stack (this work), compared with textured boron emitters passivated by thermal  $\text{SiO}_2$ ,<sup>67</sup> ALD  $\text{TiO}_2$ ,<sup>68</sup> ALD  $\text{Al}_2\text{O}_3/\text{PECVD SiN}_x$  stack,<sup>69</sup> PEALD  $\text{Al}_2\text{O}_3/\text{PECVD SiN}_x$  stack (lab-type PEALD tool),<sup>72,73</sup> PECVD  $\text{AlO}_x/\text{SiN}_x$  stack,<sup>70</sup> and PECVD  $\text{SiO}_x/\text{SiN}_x$  stack.<sup>71</sup> The error bars correspond to the standard deviation of 40 data points (eight samples and five points/sample) measured

has been achieved in this work by industrial tube-type PEALD  $\text{Al}_2\text{O}_3$  and PECVD  $\text{SiN}_x$  stack. The  $J_{0e}$  values obtained in this work are at least a factor of two lower compared with results reported for textured boron emitters passivated by thermal  $\text{SiO}_2$ ,<sup>67</sup> ALD  $\text{TiO}_2$ ,<sup>68</sup> ALD  $\text{Al}_2\text{O}_3/\text{PECVD SiN}_x$  stack,<sup>69</sup> PECVD  $\text{AlO}_x/\text{SiN}_x$  stack,<sup>70</sup> and PECVD  $\text{SiO}_x/\text{SiN}_x$  stack.<sup>71</sup> This result is comparable with the lab-type PEALD  $\text{Al}_2\text{O}_3/\text{PECVD SiN}_x$  stack,<sup>72,73</sup> demonstrating that the industrial-scale PEALD tool can provide the same high-quality layers as obtained in the literature by the lab-type PEALD tools.



**FIGURE 7** Measured interface defect density  $D_{it}(E)$  at the c-Si/ $\text{Al}_2\text{O}_3$  interface as a function of interface trap energy ( $E_t$ ) with respect to silicon's valence band energy ( $E_v$ ) for the  $\text{Al}_2\text{O}_3$  (10 nm) passivated undiffused n-type c-Si sample after firing and light soaking

### 3.2 | Electronic properties of the c-Si/PEALD $\text{Al}_2\text{O}_3$ interface

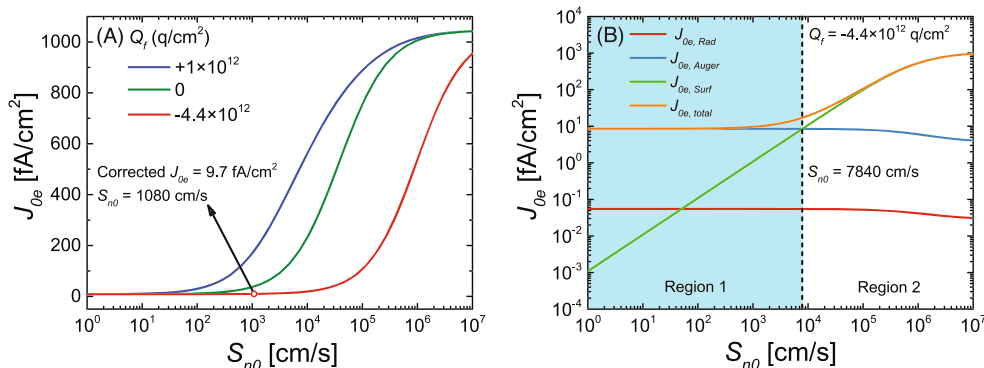
To understand the surface passivation mechanism of the developed tube-type PEALD  $\text{Al}_2\text{O}_3$  film in more detail, contactless corona-voltage measurements were carried out on undiffused silicon samples after firing and light soaking. The measured interface defect density  $D_{it}(E)$  at the c-Si/ $\text{Al}_2\text{O}_3$  interface as a function of interface trap energy ( $E_t$ ) with respect to silicon's valence band energy ( $E_v$ ) for the  $\text{Al}_2\text{O}_3$  (10 nm) passivated un-diffused n-type c-Si sample after firing and light soaking is shown in Figure 7. A  $D_{it}$  at midgap of  $1.1 \times 10^{11} \text{ cm}^{-2} \text{ eV}^{-1}$  and an average  $Q_f$  of  $-4.4 \times 10^{12} \text{ q/cm}^2$  were obtained, indicating an excellent chemical passivation and field-effect passivation by the tube-type PEALD  $\text{Al}_2\text{O}_3$  process. For comparison, a summary of typical  $D_{it}$  and  $Q_f$  values reported in the literature for  $\text{Al}_2\text{O}_3$  films grown by various ALD methods is listed in Table 1. As can be seen from Table 1, the  $D_{it}$  and  $Q_f$  values obtained from the developed industrial tube-type PEALD  $\text{Al}_2\text{O}_3$  in this work are comparable with the state-of-the-art laboratory results by the remote plasma PEALD technology. Table 1 also clearly illustrates that PEALD can achieve significantly higher negative fixed charge densities than thermal or  $\text{O}_3$  ALD. As field-effect passivation scales with the square of the fixed charge density, this improves surface passivation of a factor of 3.4 compared with thermal ALD and 1.7 compared with  $\text{O}_3$ -ALD.

### 3.3 | Simulated $J_{0e}$

Using the experimentally determined electronic interface parameters and the measured dopant profile, we quantified the  $J_{0e}$  using EDNA

**TABLE 1** A comparison of  $D_{it}$  and  $Q_f$  for  $\text{Al}_2\text{O}_3$  under different anneal conditions and deposition methods

Deposition method	Anneal condition	$Q_f$ (q/cm <sup>2</sup> )	$D_{it}$ (cm <sup>-2</sup> eV <sup>-1</sup> )	Ref.
PEALD (remote-plasma)	Annealed (400°C), N <sub>2</sub> , 10 min	$-5.8 \times 10^{12}$	$1 \times 10^{11}$	Dingemans et al. <sup>43</sup>
O <sub>3</sub> -ALD		$-3.4 \times 10^{12}$	$1 \times 10^{11}$	
H <sub>2</sub> O-ALD		$-2.4 \times 10^{12}$	$1 \times 10^{11}$	
Industrial tube-type PEALD (direct-plasma)	Fired (800°C) + light-soaked, air, 30s	$-4.5 \times 10^{12}$	$1.1 \times 10^{11}$	This work
		$-4.3 \times 10^{12}$	$1.8 \times 10^{11}$	
		$-4.4 \times 10^{12}$	$1.1 \times 10^{11}$	

**FIGURE 8** (A) Simulated  $J_{0e}$  as a function of the electron surface recombination velocity ( $S_{n0}$ ) and the fixed charge density ( $Q_f$ ) for symmetrically boron diffused emitter lifetime samples (emitter sheet resistance of 104  $\Omega/\text{sq}$ ); (B) simulated  $J_{0e}$  loss analysis by various recombination mechanisms as a function of  $S_{n0}$ . The lifetime samples were symmetrically passivated by tube-type PEALD  $\text{Al}_2\text{O}_3$ 

2. At the boron diffused emitter, the electron surface recombination velocity ( $S_{n0}$ ) was introduced to embody and quantify the recombination activity of the interface.  $S_{n0}$  was defined as<sup>74–76</sup>:

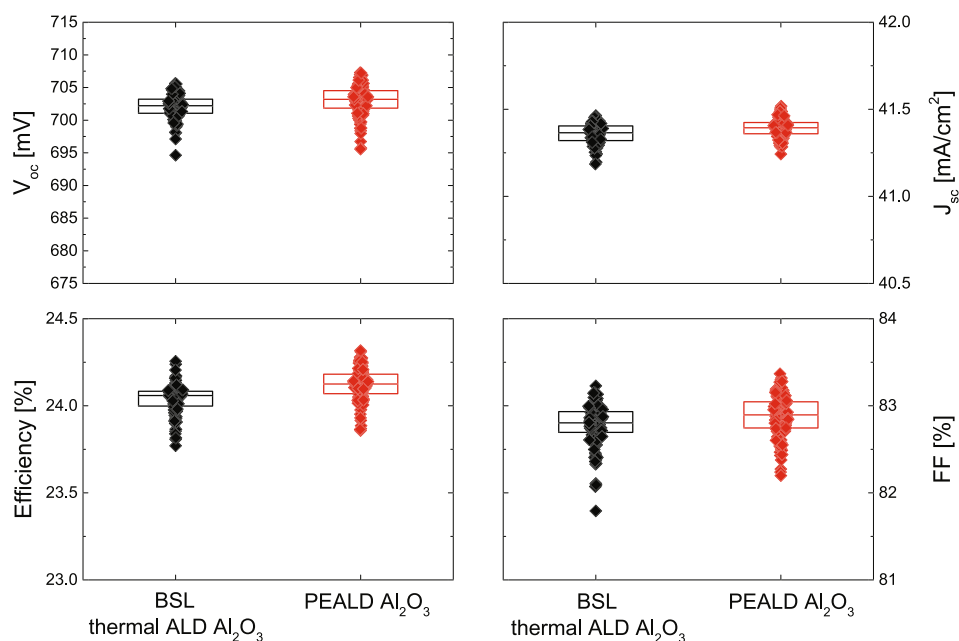
$$S_{n0} = kT\sigma_n v_{th} D_{it}(E) \quad (2)$$

where  $k$  is the Boltzmann constant,  $T$  is the temperature in Kelvin,  $\sigma_n$  is the electron capture coefficient, and  $v_{th}$  is the carrier mean thermal velocity,  $D_{it}(E)$  is the interface defect distribution. Hence, the electron capture coefficient  $\sigma_n$  can be extracted when  $S_{n0}$  was fitted to match the measured  $J_{0e}$  of the sample. The simulated  $J_{0e}$  as a function of  $S_{n0}$  and the simulated  $J_{0e}$  loss analysis by various recombination mechanisms as a function of  $S_{n0}$  are shown in Figure 8A and Figure 8B, respectively.

As shown in Figure 8A,  $Q_f$  has a strong impact on the boron emitter passivation. A high negative  $Q_f$  is beneficial for achieving good boron emitter passivation. To further understand the underlying mechanism,  $J_{0e}$  loss analysis with the contributing recombination mechanisms as a function of  $S_{n0}$  was carried out and the results are shown in Figure 8B. As can be seen from Figure 8B, the contribution from radiative recombination ( $J_{0e,Rad}$ ) is very small and negligible. As previously mentioned, SRH recombination in the emitter was not taken into account in this work. The total  $J_{0e}$  ( $J_{0e,total}$ ) was mainly dominated by the Auger recombination ( $J_{0e,Auger}$ ) and surface

recombination by the SRH recombination ( $J_{0e,SRH}$ ). A crossover point can be seen where  $J_{0e,Auger}$  and  $J_{0e,SRH}$  are equal which is at an  $S_{n0}$  value of around 7840 cm/s. For  $S_{n0}$  values below 7840 cm/s (Region 1),  $J_{0e}$  is dominated by Auger recombination and is not very sensitive to changes in  $S_{n0}$ . For  $S_{n0}$  values above 7840 cm/s (Region 2), surface recombination becomes the primary limiting loss mechanism of  $J_{0e}$ . The slight reduction in Auger, radiative, and SRH recombination for very high  $S_{n0}$  values is due to a reduction in the minority carrier concentration in the boron emitter due to increasingly large recombination at the surface. From Figure 8A, we can see that  $J_{0e}$  saturates to a minimum value  $J_{0e,min}$  of 8.6 fA/cm<sup>2</sup>. In the previous part, the measured  $J_{0e}$  from lifetime samples was from 15 to 19 fA/cm<sup>2</sup>. Since the simulations presented in Figure 8 are done in 1D, the experimental  $J_{0e}$  values should be corrected for surface area using the experimentally determined area enhancement factor of  $\sim 1.5$  for pyramid textured surfaces.<sup>77,78</sup> Hence, the corrected  $J_{0e}$  is in the range of 9.7 to 13 fA/cm<sup>2</sup>, and the corresponding  $S_{n0}$  is in the range of 1080 to 3750 cm/s. These values are located in Region 1, which indicates that  $J_{0e}$  is limited by the Auger recombination and excellent emitter surface passivation was achieved by the developed tube-type PEALD  $\text{Al}_2\text{O}_3$ . To verify the accuracy of the simulation, the  $\sigma_n$  was calculated based on Equation (2) and the measured energy-dependent  $D_{it}(E)$ . The corresponding value of  $(2-9) \times 10^{-15}$  cm<sup>2</sup> is consistent with the  $\sigma_n$  range reported for the Si/ $\text{Al}_2\text{O}_3$  interface by Werner et al.<sup>79</sup> and Saint-Cast et al.<sup>80</sup>





**FIGURE 9** Cell performance metrics of TOPCon samples with the newly developed industrial tube-type PEALD Al<sub>2</sub>O<sub>3</sub>

	Efficiency (%)	V <sub>oc</sub> (mV)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	FF (%)
BSL (thermal ALD Al <sub>2</sub> O <sub>3</sub> )	24.04	702	41.36	82.8
PEALD Al <sub>2</sub> O <sub>3</sub>	24.1	703	41.39	82.9
Best cell	24.3	707	41.41	83.1
Certified cell	24	709	40.1	84.4

**TABLE 2** Summary of the *I-V* results, based on the batch average value (100–150 cells)

### 3.4 | Solar cell performance

To verify the performance of the newly developed industrial tube-type PEALD Al<sub>2</sub>O<sub>3</sub> passivation at the device level, TOPCon cells were fabricated based on the industrial process flow shown in Figure 2. The measured *I-V* parameters are shown in Figure 9 and the batch average values are summarized in Table 2. An average cell efficiency of 24.1% was achieved with a V<sub>oc</sub> of 703 mV. The average V<sub>oc</sub> was 1 mV higher than the baseline group with the state-of-the-art thermal ALD Al<sub>2</sub>O<sub>3</sub>. For the best cell, a V<sub>oc</sub> up to 707 mV was achieved. A certified cell result of 24% by the National Institute of Metrology China is also included Table 2, with a bifacility >85%. The lower current and higher fill factor for the calibrated cell likely resulted from a difference in contacting and reflection of the measurement chuck between the two measurements. This indicates that the developed industrial tube-type PEALD Al<sub>2</sub>O<sub>3</sub> and PECVD SiN<sub>x</sub> stack passivated the textured boron emitter effectively at the device level. This could greatly help reduce the manufacturing cost for TOPCon solar cells and foster its commercialization.

## 4 | CONCLUSION

In conclusion, we demonstrated that the champion lab-scale surface passivation can now be achieved in a new tube-type industrial PEALD

reactor. State-of-the-art results were obtained on industrial textured boron emitter with a sheet resistance of 104 Ω/sq with J<sub>0e</sub> values down to 15 fA/cm<sup>2</sup> and iV<sub>oc</sub> values up to 721 mV. The results improve upon earlier results for textured boron emitters passivated by thermal SiO<sub>2</sub>, ALD TiO<sub>2</sub>, ALD Al<sub>2</sub>O<sub>3</sub>/PECVD SiN<sub>x</sub> stack, PECVD AlO<sub>x</sub>/SiN<sub>x</sub> stack, and PECVD SiO<sub>x</sub>/SiN<sub>x</sub> stack. The tube-type PEALD Al<sub>2</sub>O<sub>3</sub> films had a D<sub>it</sub> of 1.1 × 10<sup>11</sup> cm<sup>-2</sup> eV<sup>-1</sup> and Q<sub>f</sub> of -4.5 × 10<sup>12</sup> q/cm<sup>2</sup> on undiffused c-Si, indicating an excellent chemical passivation and field-effect passivation comparable with the state-of-the-art laboratory results by the remote plasma PEALD technology. Simulation results showed that the obtained J<sub>0e</sub> was quite close to its intrinsic limit, where the J<sub>0e</sub> was solely ruled by Auger recombination. Lastly, the tube-type PEALD Al<sub>2</sub>O<sub>3</sub> films were applied to industrial TOPCon solar cells where an average cell efficiency above 24% with a maximum V<sub>oc</sub> of 707 mV was obtained. This work opens a new route for mass production of high-efficiency industrial TOPCon solar cells that are not limited by recombination at Al<sub>2</sub>O<sub>3</sub> passivated highly doped boron emitter surface with a lean and cost-effective method. This tube-type PEALD process can easily be integrated in tube-based PECVD systems and therefore significantly simplifies the manufacturing complexity and reduces cost for commercial TOPCon solar cells.

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## DATA AVAILABILITY STATEMENT

The data that support the findings of this study are available from the corresponding author upon reasonable request.

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